



**Fauske & Associates, Inc.**

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From: Martin G. Plys, FAI

Subject: **Flammability and Combustion of H<sub>2</sub>, Air or O<sub>2</sub>, and Ar Gas Mixtures**

Flammability and combustion characteristics for hydrogen, air or oxygen, and argon are discussed here to assist evaluation for the KE sludge removal process with an argon gas purge.

For the case where a large diameter container (LDC) is purged by Ar, but H<sub>2</sub> and O<sub>2</sub> may evolve, flammability data given by Coward and Jones are available for the case of the ratio of O<sub>2</sub>/Ar equal to the ratio of O<sub>2</sub>/(N<sub>2</sub>+Ar) in air, which is 0.21/0.79. The lean flammability limit is 3.2% H<sub>2</sub>, 76.5% Ar, and 20.3% O<sub>2</sub>. This is slightly lower than the value of 4% hydrogen in air. The rich flammability limit is 76.4% H<sub>2</sub>, 18.6% Ar, and 5% O<sub>2</sub> which is exactly the same oxygen content for the case of hydrogen in air. For practical purposes the rich limit of 5% O<sub>2</sub> is the value of interest to the project and is recommended except as follows.

A reference cited by Coward and Jones, Van Heiningen 1936, provides flammability data for the case of H<sub>2</sub>-Air-Ar mixtures, which may be pertinent to the case of an LDC containing only hydrogen and argon but with in-leakage of air or incomplete purging of air. These data are reproduced in Figures 1, 2, and 3, which provide the overall flammability limit, a closeup of the lean limit, and the equivalent oxygen at the rich limit, respectively. Both lean and rich limit data for low Ar concentrations lie between today's known upward and downward propagation limits, and are an artifact of the experiment size and ignition location. Thus the fuel concentration decreases toward 4% on the lean limit as Ar is added, and the oxygen concentration also decreases. However, the oxygen concentration goes below 5% near 50% Ar, an unexpected result, and is about 4.1% at 70% Ar. This cannot be explained by the apparatus alone and cannot be discounted for industrial application. Thus, for the case of air ingress into an existing H<sub>2</sub>-Ar mixture, a lower oxygen limit between 4% and 5% is recommended by using a linear fit:  $x_{O_2} = 5 - (x_{Ar} - 50)/20$  where  $x$  is mole percent and  $50\% < x_{Ar} < 70\%$ . Use 5% O<sub>2</sub> when  $x_{Ar} < 50\%$  and use 4% O<sub>2</sub> when  $x_{Ar} > 70\%$ . However, the mixture is completely inert when  $x_{Ar} > 76\%$ .

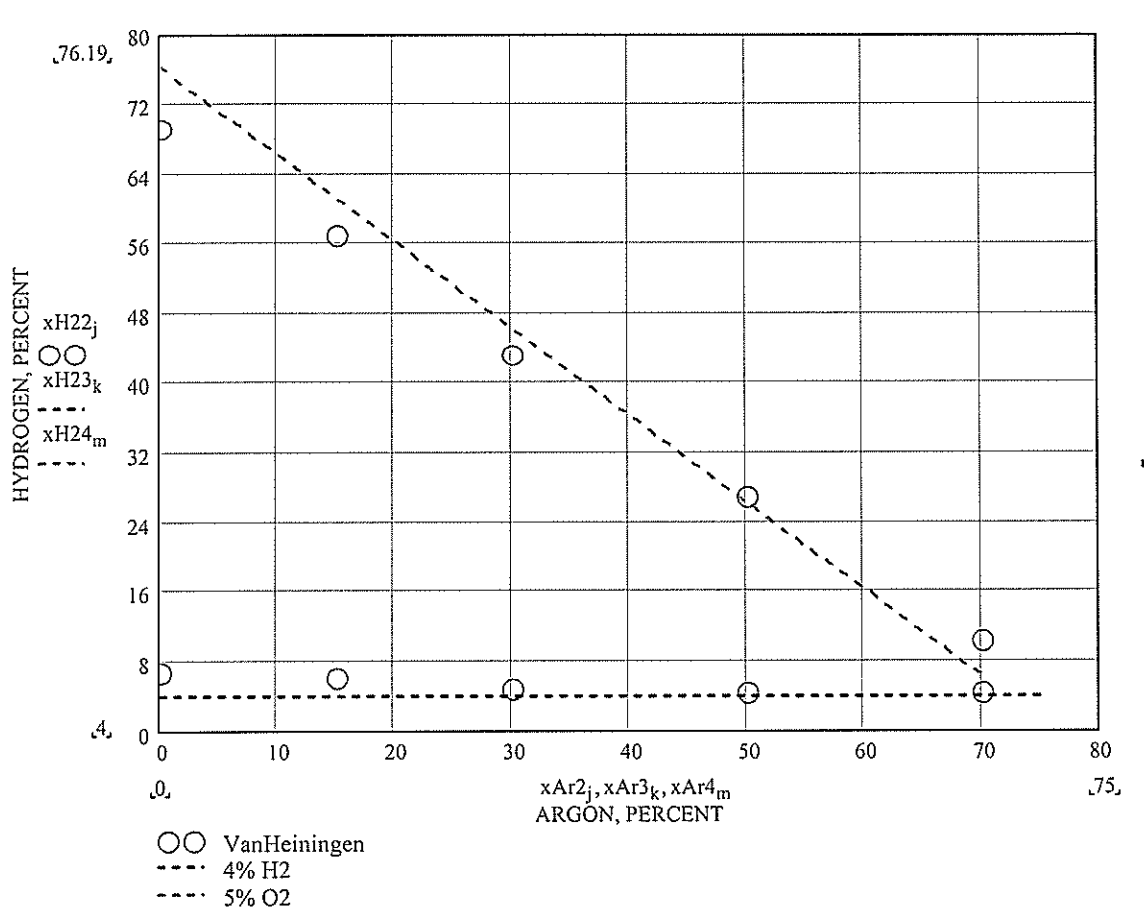
Lastly, it should be noted that because Ar has a lower heat capacity than air, the post-combustion pressure of a flammable mixture is higher with Ar than with air. Figure 4 provides the post-combustion pressure for a set of mixtures with various O<sub>2</sub> concentrations as indicated, beginning with a minimum stoichiometric quantity of hydrogen, so that rich mixture results are shown. Complete combustion is assumed in the absence of data near the rich limit.

References:

H.F. Coward and G.W. Jones, Limits of Flammability of Gases and Vapors, U.S. Bureau of Mines Bulletin 503, 1952.

J. Van Heiningen, Explosion Limits I: On the Influence of Argon, Nitrogen, Helium, and Carbon Dioxide on the Explosion Limits of Hydrogen, Carbon Monoxide, Methane, and Butane in Air, Recueil des Travaux Chimiques des Pays Bas, Vol. 55, pp. 65-75, 1936.

Figure 1. Flammability Limit Data for H<sub>2</sub>-Air-Ar mixtures, Van Heiningen, 1936. For reference lines of 4% H<sub>2</sub> and 5% O<sub>2</sub> are drawn.



Figures 2 and 3. Closeup of Figure 1 lean flammability limit (top) and oxygen percentage at the rich flammability limit (bottom).

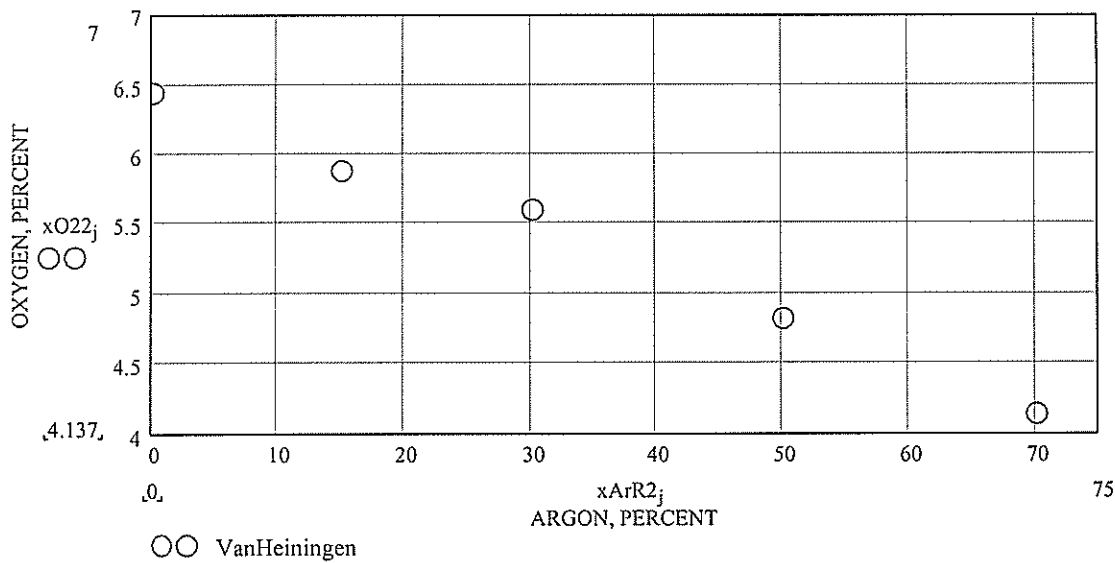
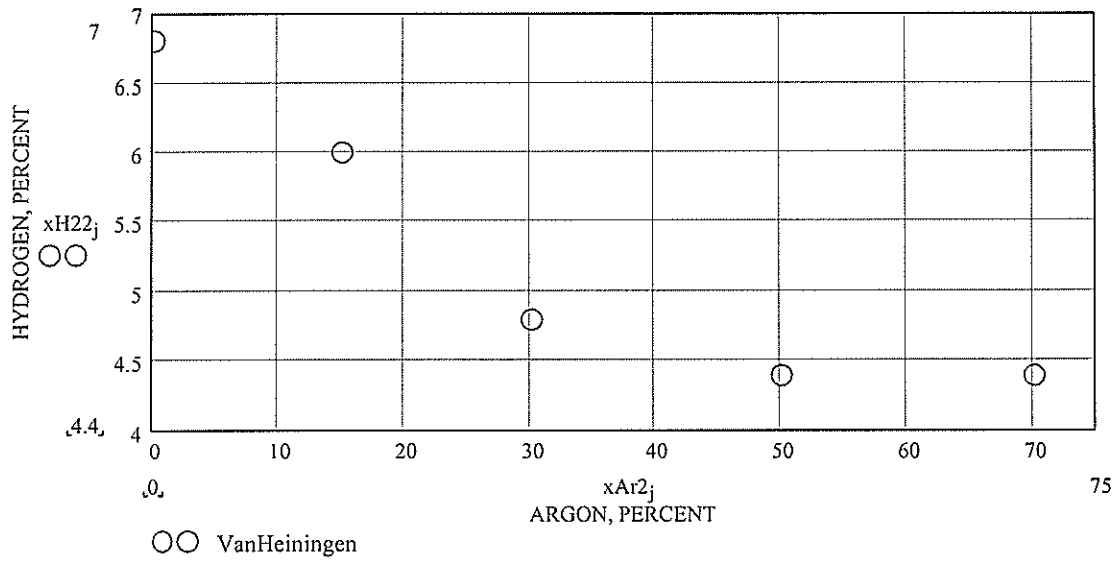


Figure 4. Post-combustion pressure for H<sub>2</sub>-O<sub>2</sub>-Ar mixtures with various O<sub>2</sub> proportions and a minimum H<sub>2</sub> stoichiometric content.

